



INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

<p>(51) International Patent Classification 6 :  <b>B23K 20/12, B29C 65/06</b></p>	<p><b>A1</b></p>	<p>(11) International Publication Number: <b>WO 95/26254</b></p> <p>(43) International Publication Date: <b>5 October 1995 (05.10.95)</b></p>						
<p>(21) International Application Number: <b>PCT/NO95/00005</b></p> <p>(22) International Filing Date: <b>5 January 1995 (05.01.95)</b></p> <p>(30) Priority Data:</p> <table style="width: 100%; border: none;"> <tr> <td style="width: 33%;">941144</td> <td style="width: 33%;">28 March 1994 (28.03.94)</td> <td style="width: 33%;">NO</td> </tr> <tr> <td>942790</td> <td>27 July 1994 (27.07.94)</td> <td>NO</td> </tr> </table> <p>(71) Applicant (for all designated States except US): <b>NORSK HYDRO A.S [NO/NO]; N-0240 Oslo (NO).</b></p> <p>(72) Inventors; and</p> <p>(75) Inventors/Applicants (for US only): <b>MIDLING, Ole, Terje [NO/NO]; Ivar Aasenveg 26, N-4250 Kopervik (NO). MORLEY, Edward, James [GB/NO]; Nordstokke, N-4250 Kopervik (NO). SANDVIK, Anders [NO/NO]; Vestre, N-5474 Skjold (NO).</b></p> <p>(74) Agent: <b>RICANEK, Ivan; Norsk Hydro a.s, N-0240 Oslo (NO).</b></p>		941144	28 March 1994 (28.03.94)	NO	942790	27 July 1994 (27.07.94)	NO	<p>(81) Designated States: <b>AM, AT, AU, BB, BG, BR, BY, CA, CH, CN, CZ, DE, DK, EE, ES, FI, GB, GE, HU, JP, KE, KG, KP, KR, KZ, LK, LR, LT, LU, LV, MD, MG, MN, MW, MX, NL, NO, NZ, PL, PT, RO, RU, SD, SE, SI, SK, TJ, TT, UA, US, UZ, VN, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, ML, MR, NE, SN, TD, TG), ARIPO patent (KE, MW, SD, SZ).</b></p> <p><b>Published</b>  <i>With international search report.</i></p>
941144	28 March 1994 (28.03.94)	NO						
942790	27 July 1994 (27.07.94)	NO						
<p>(54) Title: <b>FRICTION STIR WELDING</b></p> <p>(57) Abstract</p> <p>An improved method of friction stir welding is based on enhanced flow of plasticised material both perpendicularly and vertically to the longitudinal extension of the adjacent assembled members by exposing the created plasticised material to a perpendicular pressure along the surface of the members and causing simultaneous material flow along the probe pin in the vertical direction allowing the plasticised material to solidify behind the probe. A non-consumable probe (1) is provided comprising a concave bottom part (23) with an interchangeable pin (24) having surface of threaded configuration and in a preferred embodiment comprising two or more laterally protruding blades.</p>								

**FOR THE PURPOSES OF INFORMATION ONLY**

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AT	Austria	GB	United Kingdom	MR	Mauritania
AU	Australia	GE	Georgia	MW	Malawi
BB	Barbados	GN	Guinea	NE	Niger
BE	Belgium	GR	Greece	NL	Netherlands
BF	Burkina Faso	HU	Hungary	NO	Norway
BG	Bulgaria	IE	Ireland	NZ	New Zealand
BJ	Benin	IT	Italy	PL	Poland
BR	Brazil	JP	Japan	PT	Portugal
BY	Belarus	KE	Kenya	RO	Romania
CA	Canada	KG	Kyrgyzstan	RU	Russian Federation
CF	Central African Republic	KP	Democratic People's Republic of Korea	SD	Sudan
CG	Congo	KR	Republic of Korea	SE	Sweden
CH	Switzerland	KZ	Kazakhstan	SI	Slovenia
CI	Côte d'Ivoire	LI	Liechtenstein	SK	Slovakia
CM	Cameroon	LK	Sri Lanka	SN	Senegal
CN	China	LU	Luxembourg	TD	Chad
CS	Czechoslovakia	LV	Latvia	TG	Togo
CZ	Czech Republic	MC	Monaco	TJ	Tajikistan
DE	Germany	MD	Republic of Moldova	TT	Trinidad and Tobago
DK	Denmark	MG	Madagascar	UA	Ukraine
ES	Spain	ML	Mali	US	United States of America
FI	Finland	MN	Mongolia	UZ	Uzbekistan
FR	France			VN	Viet Nam
GA	Gabon				

### Friction stir welding

The present invention relates to a method of friction welding for joining of (metal) members and more particularly to so-called friction stir welding based on a relative rubbing movement between a probe of harder material and members to be joined. The present invention also is directed to an improved tool to be applied in the friction welding process.

Friction welding based on the principle of "rubbing" of articles to be joined together so as to generate a sufficient amount of heat, thus generating plasticised conditions in the adjacent surfaces, has been known and practised for several decades. The frictional heat is generated solely by the two to be joined components. However, the resulting weld seams suffer from a number of disadvantages inherent in the applied processes. The main drawback which considerably limits the applicability of friction welding is that at least one of the components to be welded has to be axis-symmetric. Consequently, such process is not applicable for e.g. structural applications requesting provision of longitudinal continuous welds.

The improved version of this welding, so-called friction stir welding, is known from WO93/10935. A probe (third body) of a harder material than the treated workpieces is applied in the welding process. Friction stir welding is based on a relative cyclic movement between the probe and the workpieces, urging the probe and workpieces together to create a plasticised region in the workpiece region due to generated frictional heat, stopping the relative cyclic movement and allowing the plasticised material to solidify. Thus no heat is generated due to a relative motion between the workpieces to be joined. The method is illustrated by

several examples of different workpiece materials (plastics, metals), applications (reparation of cracks, sealing, joining) and embodiments of the applied probe.

Neither the above disclosed method and apparatus, when applied for joining of extruded shapes into structures for critical applications, can meet the request for high integrity welds free from voids and proper metallurgical bonding of structural parts, nor a demand for provision of welds in a lap configuration.

In order to achieve a proper consolidation of the weld metal the probe bottom part (shoulder) must maintain during the whole welding operation (forward movement) in an intimate contact with surface of the joined members. If the probe shoulder during this forward movement even temporarily "lifts" from the surface a small amount of plasticised welding material will be expelled behind the probe thus causing occurrence of voids in the weld since there is no available material to fill the vacant space after the expelled material.

Furthermore there is another limitation connected to use of "smooth" welding probe known from the prior art, namely low welding speeds are required in order to achieve a sufficient frictional heating of the material (contact time between the probe and the joined members), and to ensure a sufficient flow of the plasticised welding material.

It is therefore an object of the present invention to provide an improved method of friction stir welding, ensuring high integrity welds free from voids and exhibiting a smooth quality surface.

A further object of the invention is to improve the present known friction stir butt welding method to provide also lap welds and three or more components joint configuration.

Another object of the present invention is to provide a new type of probe ensuring uniform homogenized weld seams exhibiting reduced heat affected zone.

The above and other objects are achieved in accordance with the present invention by provision of a method for friction stir welding and an apparatus (probe) as defined in the accompanying claims 1 and 7, respectively.

Other objects, specific features and advantages of the present invention will be apparent from the following detailed descriptions of preferred embodiments with reference to the accompanying drawings, Figs. 1-5, where:

- Fig. 1 is a schematic perspective view of the welding apparatus/-process employable in the present invention,
- Fig. 2 illustrates in an enlarged cross-sectional (partial) view the configuration of the two components probe,
- Fig. 3 shows schematically principal features of the novel friction stir welding,
- Fig. 4 shows graphically the optimal relation between welding and rotational speed and applied pressure on the probe, and
- Figs. 5a-e are fragmentary, schematic perspective views of different types of the provided weld seams.

Referring to the drawings, particularly to Fig. 1, a non-consumable probe 1 comprising a rotational cylindrical body 2 having an upper part 22 being connected to a power source, e.g. an engine (not shown in the drawing), and a bottom part 23 provided with a separate pin 24, is applied for joining (welding) of two butt to butt arranged members (metal plates) 3 and 4. By insertion of the probe 1 between the members 3,4 under pressure and rotation in order to provide adequate frictional heating a butt seam weld 5 is subsequently provided during a transitional movement along the butt arranged members.

The special inventive configuration of the composite two parts probe 1, the bottom part 23 (shoulder) of the probe and outer shape (configuration) of the applied pin 24 according to the present invention is more apparent from Fig. 2, where the bottom part 23 of the rotational cylindrical body 2 exhibits a concave surface, while the pin's 24 outer surface is provided with alternately protruding and recessed parts along its longitudinal axis.

Even if a conventional screw thread on the outer pin surface is applicable and will improve the weld quality, in a preferred embodiment of the probe pin the surface configuration, as illustrated in the Figure, comprises advantageously two or more separate blades 25 vertically disposed and laterally protruding from the central portion of the pin.

Microstructure of welding seams provided by this novel type of the pin exhibits sound joints composed of interlocked plasticised segments of the joined members with minimal material turbulence.

The composite design of the applied probe 1 comprising a separate probe pin compared to the monolithic design of the previously known probes presents several advantages. Firstly, the tool (probe) is capable of adjustment of the depth of pin insertion, thus offering a process flexibility. Secondly, the pin portion can be easily interchanged between different tool units (shoulder/holder) and thus adapted for welding of members having various wall thickness.

The innovative features of the new tool and improved process of friction stir welding will be readily understood from the schematical sketch of the probe and welding performance as illustrated in Fig. 3, where  $W$  denominates the thickness of the welded members,  $\omega$  welding speed,  $R$  radius of curvature of the concave probe shoulder,  $F$  downward force (pressure) applied on the probe,  $r_s$  probe shoulder radius, and  $t$  represents "undercut" of the shoulder into the welded material.

The concave bottom surface 23 of the probe 1 exhibiting slight inclination in relation normal to the welding surfaces combined with the above described screw configuration of the pin 24 (not shown in the Figure) ensures that the plasticised material is driven both vertically and laterally in a weld zone, thereby transforming metal between different levels across the weld profile. The concave shape of the probe shoulder provides a certain non-symmetric compression on the surface of the members resulting in vertical flow/transition of material. This in co-operation with horizontal movement of material due to the pin's outer configuration results in high quality void free seams.

Fig. 4 illustrates schematically an optimum relation between a downward pressure  $\frac{F}{\pi r_s^2}$

in  $N/mm^2$  applied on the probe and the actual welding speed  $\omega$  (mm/min) at different rotational speeds ensuring a sound void free weld having a smooth surface. The actual values of optimal pressure/welding speed are dependent on several factors, e.g. applied material of the joined members (Al-alloys), shoulder geometry etc.

Several welding trials conducted with probes of different diameters show that reduction of the probe shoulder's diameter related to the actual wall thickness of the joined members has a beneficial effect on the quality of the provided joints/seams besides possibility of increasing the welding speed.

Thus, reduction of the probe shoulder's diameter from 20 mm to 15 mm and further to 10 mm applied for joining of 3 mm thick flat extrusions of alloy 6082.50 allowed an increase of the welding speed from 0.3 m/min to 0.8 m/min achieving high quality porefree welds exhibiting reduced HAZ (heat affected zone). This is a combined result of decreased heat input and its focusing towards the vicinity of the formed seam allowing for increase of the welding speed and reduced downward force applied on the probe resulting in distortion free welded structures.

A simple formula defining an optimal relation between the radius of the probe shoulder ( $r_s$ ) and the wall thickness of the welded members  $W$  will be:

$$5 \frac{W}{2} \geq r_s \geq \frac{W}{2}$$

The material of the probe is harder than the workpieces/members to be joined. Typically for application on aluminium (alloy) members the material should exhibit a good strength at elevated temperatures, e.g. hot work steel, high speed steel or cermet material can be applied.

Figs. 5a-e display schematically in fragmentary perspective views different types of welds provided by the method and probe according to the present invention, where

Fig. 5a shows a conventional butt weld, Fig. 5b shows a T-section connection between two members, Fig. 5c is an overlap weld seam, Fig. 5d shows another variant of T-section composed of three members, and finally Fig. 5e illustrates provision of a corner weld between two members arranged in a normal plane to each other.

Thus application of the new and improved tool design according to the present invention allows for increased welding speeds while ensuring sufficient generation of frictional heat. This effect is achieved due to an extended contact/heating time per volume unit of the welding material and closer localization of the generated heat along the welding line. Further more substantial forging forces (pressure) are applied on the material when leaving the welding probe. Optimal combination of the above effects results in high quality welds both with regard to the metallurgical and mechanical properties due to a homogenized weld exhibiting no porosity through the whole weld cross-section.



Claims

1. A method of friction stir welding of members, particularly for joining of extruded assembled shapes, comprising steps of urging and securing the assembled members towards each other, entering the assembled members along the joining line by a probe of material harder than the material of joined members under rotating movement which generates a frictional heat, thereby creating a plasticised region in the adjacent members' material, the method further comprising a homogenization of the resulting weld seam ensured by an enhanced flow of plasticised material both perpendicularly and vertically to the longitudinal extension of the adjacent assembled members by exposing the created plasticised material to a perpendicular pressure along the surface of the members and causing simultaneous material flow along the probe pin in the vertical direction allowing the plasticised material to solidify behind the probe.
2. Method according to claim 1, characterized in that the probe bottom part (23) engages the adjacent surfaces of the members to be joined under a slight inclination from normal to welding surfaces.
3. Method according to claim 1 or 2, characterized in that the probe pin's (24) outer configuration ensures a vertical and lateral flow of the plasticised material across a weld zone.
4. Method according to any of the preceding claims, characterized in that two or more members are welded providing a T-type welding joint.

5. Method according to any of claims 1-3,  
c h a r a c t e r i z e d i n t h a t  
the provided welded seam is a lap welding joint.
6. Method according to any of claims 1-3,  
c h a r a c t e r i z e d i n t h a t  
the provided weld seam is a corner weld connecting two members arranged  
substantially at any angle to each other.
7. A non-consumable probe (1) for stir friction welding of members comprising a  
rotational, substantially cylindrical body (2), having an upper part (22) connected  
to a power source and a bottom part (23) provided with a pin (24),  
c h a r a c t e r i z e d i n t h a t  
the bottom part (23) of the probe has a concave face and the attached pin (24)  
is an interchangeable part of the probe exhibiting a threaded surface  
configuration.
8. Probe according to claim 7,  
c h a r a c t e r i z e d i n t h a t  
the pin is provided with at least a pair of vertically disposed blades laterally  
protruding from the pin's central portion.

1/3

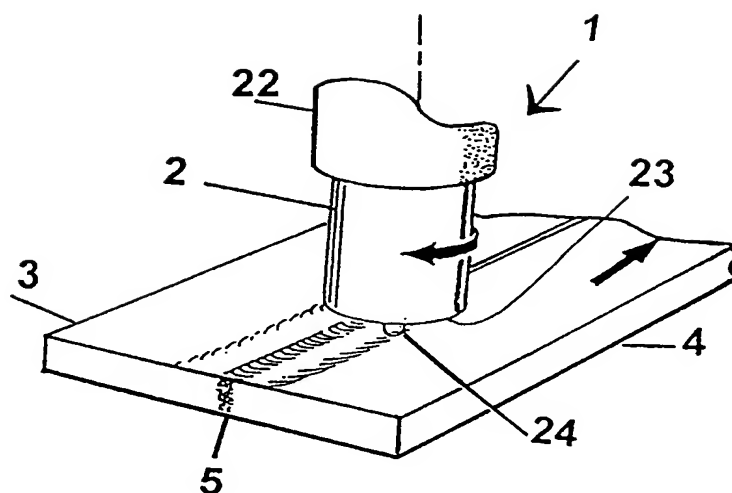


Fig. 1

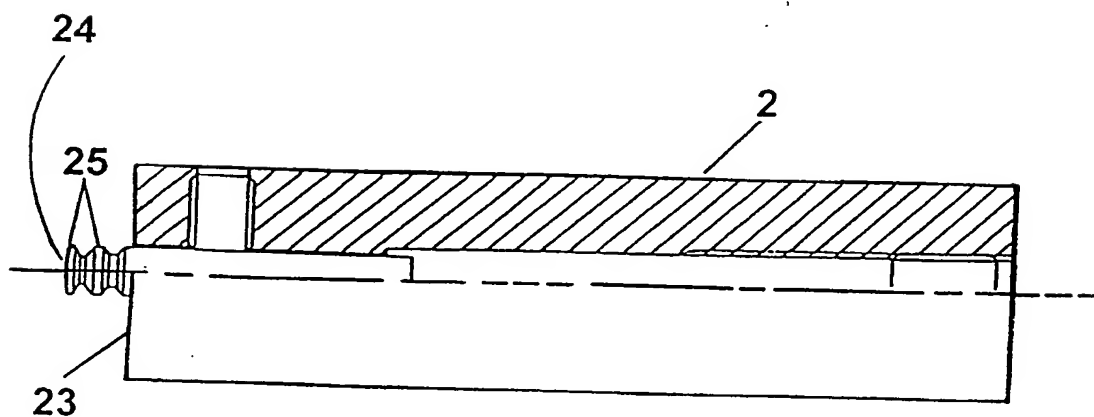


Fig. 2

SUBSTITUTE SHEET

2/3

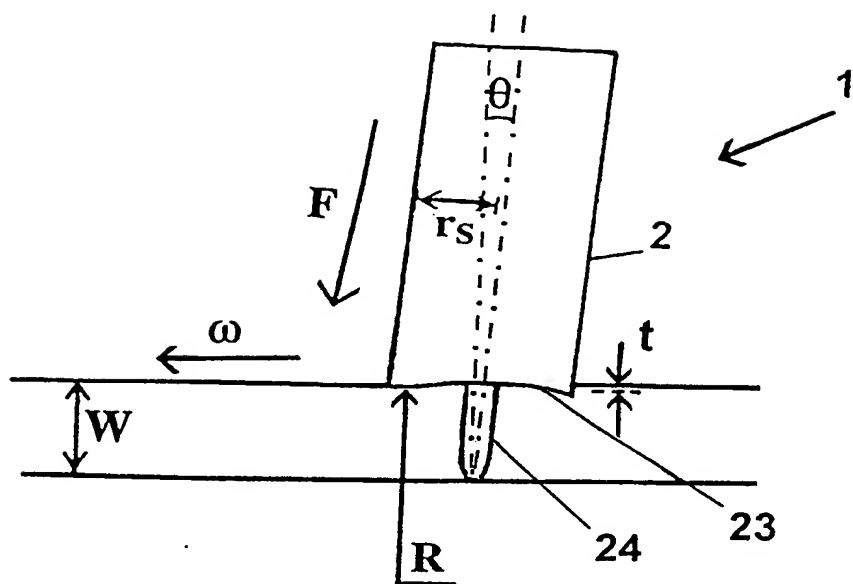


Fig. 3

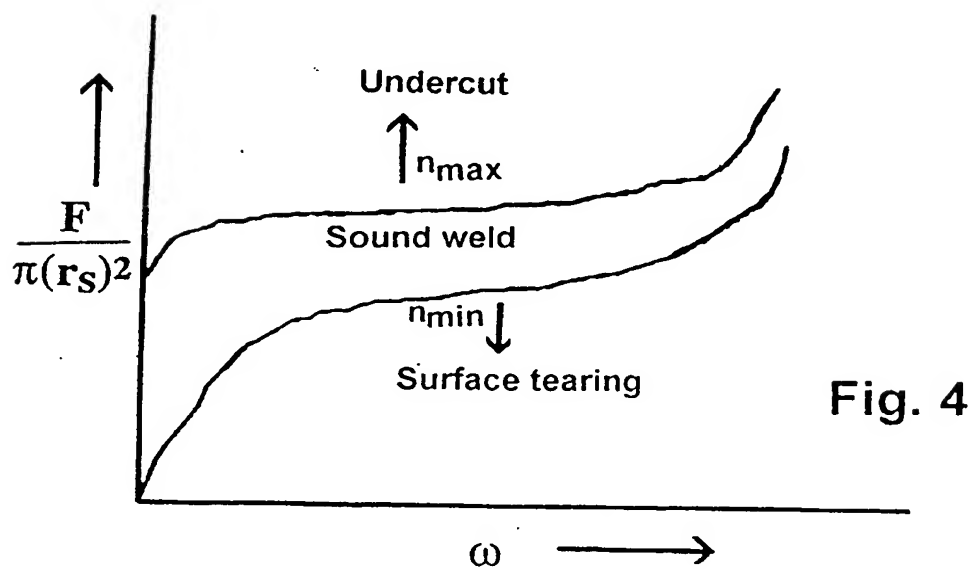


Fig. 4

SUBSTITUTE SHEET

3/3

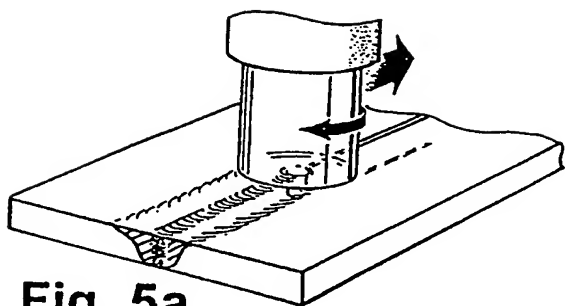


Fig. 5a

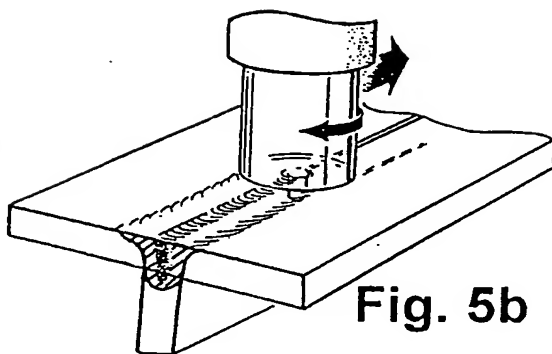


Fig. 5b

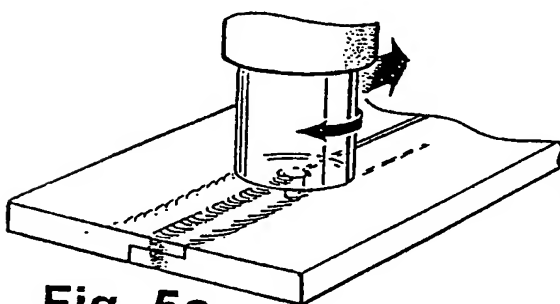


Fig. 5c

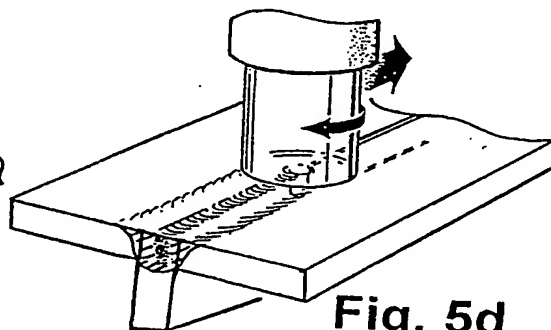


Fig. 5d

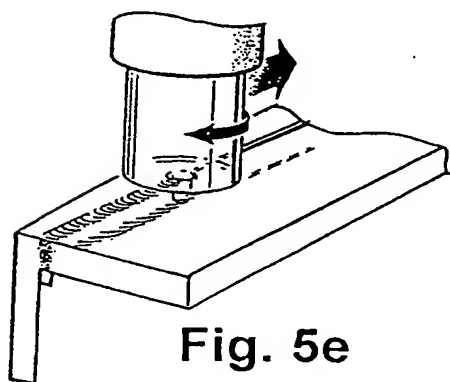


Fig. 5e

SUBSTITUTE SHEET

# INTERNATIONAL SEARCH REPORT

International application No.

PCT/NO 95/00005

## A. CLASSIFICATION OF SUBJECT MATTER

IPC6: B23K 20/12, B29C 65/06

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC6: B23K, B29C

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

SE,DK,FI,NO classes as above

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

WPAT, CLAIMS, WELDASEARCH

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	WO 9310935 A1 (THE WELDING INSTITUTE), 10 June 1993 (10.06.93)  -----	1-8

☐ Further documents are listed in the continuation of Box C. ☒ See patent family annex.

- |  |   |
|--|---|
| <p>* Special categories of cited documents:</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> | <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance: the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone</p> <p>"Y" document of particular relevance: the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art</p> <p>"&amp;" document member of the same patent family</p> |
|--|---|

Date of the actual completion of the international search	Date of mailing of the international search report
11 July 1995	'13 -07- 1995
Name and mailing address of the ISA/ Swedish Patent Office Box 5055, S-102 42 STOCKHOLM Facsimile No. +46 8 666 02 86	Authorized officer  Bertil Dahl Telephone No. +46 8 782 25 00

## INTERNATIONAL SEARCH REPORT

29/05/95

International application No.

PCT/NO 95/00005

Parent document cited in search report	Publication date	Patent family member(s)	Publication date
WO-A1- 9310935	10/06/93	AU-B- 658950	04/05/95
		AU-A- 1016495	30/03/95
		AU-A- 2952892	28/06/93
		CA-A- 2123097	10/06/93
		EP-A- 0615480	21/09/94
		EP-A- 0653265	17/05/95